

Q.

Design a suitable double-angle discontinuous strut in a steel truss to carry a working axial compressive load of 200 kN. The effective length of the strut is 2.12 m. Use a gusset plate of 20 mm thick. Assume column buckling class c. $f_y = 250$ MPa, $f_u = 400$ MPa, $\gamma_{mb} = 1.25$.

Relevant portion of the code books is enclosed.

solution :- Assuming $f_{cd} = 0.5 f_y$

$$f_{cd} = 0.5 \times 250$$

$$f_{cd} = 125 \text{ N/mm}^2$$

Effective sectional area required

$$A_e = \frac{P}{f_{cd}} = \frac{1.5 \times 200 \times 10^3}{125}$$

$$A_e = 2400 \text{ mm}^2$$

cross sectional area of a single Angle = $\frac{2400}{2} = 1200 \text{ mm}^2$

-selecting ISA 80 x 80 x 8, $A = 1221 \text{ mm}^2 > 1200 \text{ mm}^2$

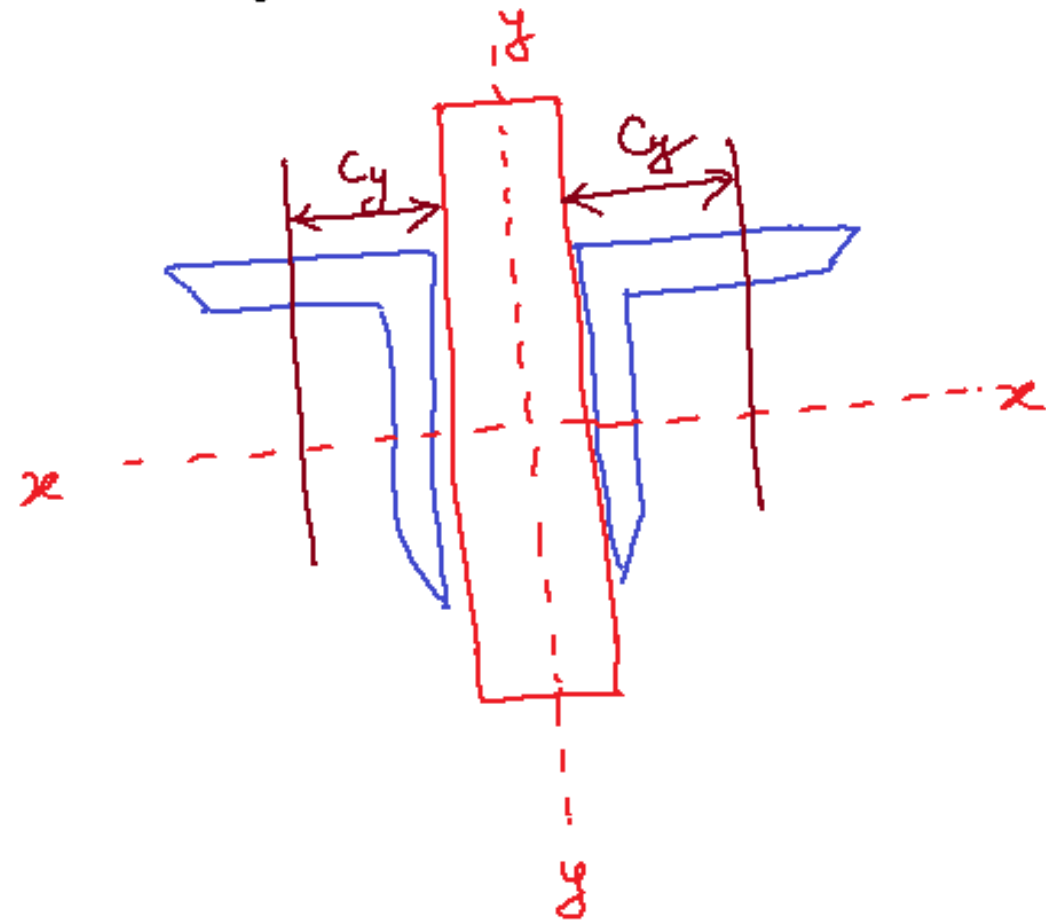
properties of ISA 80 x 80 x 8

$$C_x = C_y = 22.7 \text{ mm}$$

$$I_{xx} = I_{yy} = 72.5 \times 10^4 \text{ mm}^4$$

$$r_x = r_y = 24.4 \text{ mm}$$

- Let Angles are placed opposite side of the gusset plate



$$A' = 2A$$

$$A' = 2 \times 1221$$

$$A' = 2442 \text{ mm}^2$$

$$I'_{xx} = 2I_x$$

$$A' = 2A$$

$$r'_{xx} = \sqrt{\frac{I'_{xx}}{A'}} = \sqrt{\frac{2I_x}{2A}} = r_{xx}$$

$$\gamma'_x = \gamma_x = 24.4 \text{ mm}$$

$$\gamma'_x = 24.4 \text{ mm}$$

$$I'_y = 2 [I_y + A h^2]$$

$$I'_y = 2 \left[I_y + A \left(c_y + \frac{t_x}{2} \right)^2 \right]$$

$$I'_y = 2 \left[72.5 \times 10^4 + 1221 \times \left(22.7 + \frac{20}{2} \right)^2 \right]$$

$$I'_y = 406.12 \times 10^4 \text{ mm}^4$$

$$\delta_y' = \sqrt{\frac{I_y'}{A'}} = \sqrt{\frac{406.12 \times 10^4}{2442}}$$

$$\delta_y' = 40.78 \text{ mm}$$

$$\delta_{min}^{\circ} = (\delta_x', \delta_y')$$

$$\delta_{min}^{\circ} = (24.4 \text{ mm}, 40.78 \text{ mm})$$

$$\delta_{min}^{\circ} = 24.4 \text{ mm}$$

$$\lambda = \frac{l_e}{r_{min}} = \frac{2.12 \times 10^3}{24.4} = 86.88$$

$$\boxed{\lambda = 86.88} < 350 \quad \text{OK} \checkmark$$

from the buckling class 'c'

λ	f_{cd}
80	136
86.88	f_{cd}
90	121

$$\frac{90-80}{121-136} = \frac{90-86.88}{121-f_{cd}}$$

$$f_{cd} = 125.68 \text{ N/mm}^2$$

Design capacity, $P_d = f_{cd} \times A'$

$$P_d = (125.68 \times 2442) \times 10^{-3}$$

$$P_d = 306.91 \text{ kN}$$

$$\therefore (P_u = 300 \text{ kN}) < (P_d = 306.91 \text{ kN})$$

$\therefore$ Safe

Design of Bolted Connection

Assuming diameter of bolt = 20mm

$$d = 20 \text{ mm}$$

$$d_o = 22 \text{ mm}$$

① Design shearing strength of bolt

$$V_{dsb} = \frac{f_{ub}}{\sqrt{3} \gamma_{mb}} (n_n A_{nb} + n_s A_{sb})$$

$$V_{dsb} = \frac{400}{\sqrt{3} \times 1.25} \left(1 \times 0.78 \times \frac{\pi}{4} 20^2 + 1 \times \frac{\pi}{4} 20^2 \right) \times 10^{-3}$$

$$V_{dsb} = 103.314 \text{ kN}$$

① Design bearing strength of bolt

$$V_{dpb} = \frac{2.5 k_b (d t) f_u}{\gamma_{mb}}$$

$$e_{min} = 1.5 d_o = 33 \text{ mm}$$

$$p_{min} = 2.5 d = 50 \text{ mm}$$

Assuming

$$e = 35 \text{ mm}$$

$$p = 50 \text{ mm}$$

$$K_b = \min \left[\frac{e}{3d_o}, \frac{P}{3d_o} - 0.25, \frac{f_{ub}}{f_u}, 1 \right]$$

$$K_b = \min \left[\frac{35}{3 \times 22}, \frac{50}{3 \times 22} - 0.25, \frac{400}{410}, 1 \right]$$

$$K_b = \min [0.53, 0.507, 0.97, 1]$$

$$K_b = 0.507$$

$$t = \min [2 \times 8 \text{ mm}, 20 \text{ mm}]$$

$$t = 16 \text{ mm}$$

$$V_{dpb} = \frac{2.5 \times 0.507 \times 20 \times 16 \times 410}{1.25} \times 10^{-3}$$

$$V_{dpb} = 133.04 \text{ kN}$$

$$\text{Bolt value, } V_{db} = \min (V_{dsb}, V_{dpb})$$

$$V_{db} = 103.314 \text{ kN}$$

$$\text{No. of bolts required} = \frac{P_u}{V_{db}}$$

$$N = \frac{300}{103.314} = 2.9$$

$$N = 3$$

providing 3 bolts of 20 mm
diameter @ 50 mm c/c pitch

